

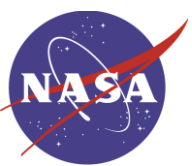
Simultaneous Communications/Tracking/Navigation for Multiple Spacecraft (in a beam) in Deep Space

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Outline of Talk

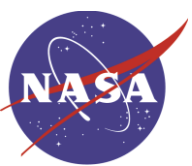
BACKGROUND AND CHALLENGES

- **NOTIONAL MARS REGIONAL NAVIGATION SATELLITE SYSTEM (MRNSS)**

SIMULTANEOUS COMMUNICATIONS/TRACKING/NAVIGATION

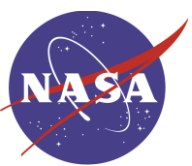
- **SIMULTANEOUS UPLINK, AND 2-WAY DOPPLER/RANGING**
- **SIMULTANEOUS DELTA-DOR: SAME BEAM INTERFEROMETRY (SBI)**

CAN SIMULTANEOUS COMMUNICATIONS/TRACKING ENABLE NEW MISSION CONCEPT AND SCIENCE?



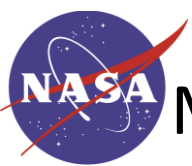
Background and Challenges (1)

- Typically one DSN ground station communicates with one spacecraft in deep space
- At Mars when multiple spacecraft are in the beam, one ground station can receive multiple downlinks (and one uplink) via MSPA, which is a static form of FDMA
- Traditional deep space tracking techniques include Doppler, ranging, and delta-DOR
- 2-Way Doppler/ranging requires tight coordination between ground and flight (Doppler compensation), and one ground station tracking one spacecraft (1-to-1)
- Delta-DOR is 1-way, but requires two ground station tracking one spacecraft (2-to-1)
- When number of missions increase, and for missions with multiple spacecraft, there might not be enough DSN antenna assets to meet missions' communications and tracking needs
- There is a desire to extend the current deep space communications and tracking techniques to support multiple spacecraft in a beam to improve the antenna usage efficiency



Background and Challenges (2)

- In 2016 we proposed a low-cost low-maintenance Mars Regional Navigation Satellite System (MRNSS) to support human Mars missions [8]:
 - Capitalize on the build-up of orbiting and surface infrastructures on Mars during the human Mars exploration era [1][2][3]
 - Leverage on a new geometric trilateration method that simultaneously performs absolute positioning and relative positioning [4][5]
 - Introduce the concept of using relative positioning that provides regional navigation services in the vicinity of a human Mars landing site (~100 km), thereby relieving the stringent requirements on orbit determination (OD) of Mars navigation satellites
 - Extend current DSN's tracking approaches of pairing one or two dedicated ground stations to one spacecraft for a period of time to simultaneously tracking of multiple Mars orbiters
 - Simultaneous Doppler/ranging [6]
 - Same Beam Interferometry [7]



Mars Regional Navigation Satellite System (MRNSS) [8]

Same Beam Interferometry (SBI) [7]

new node

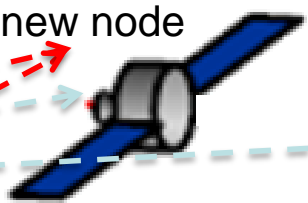
Existing Mars assets



Occasional DSN tracks



Existing Mars assets



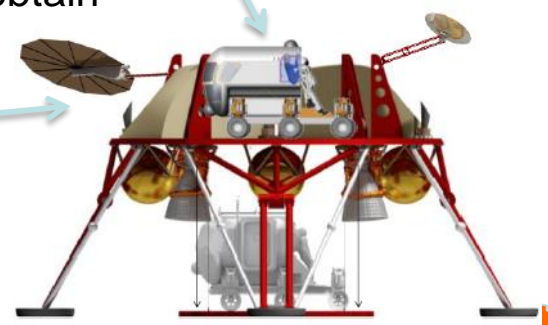
"error-canceling" node on existing Mars assets

Raw range measurements

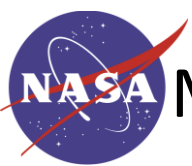
Simultaneous Doppler/ranging of orbiters within the ground antenna beamwidth [6]

"Differencing" of raw range measurements to obtain precision relative positioning [4][5]

Mars landing site



Mars landing site

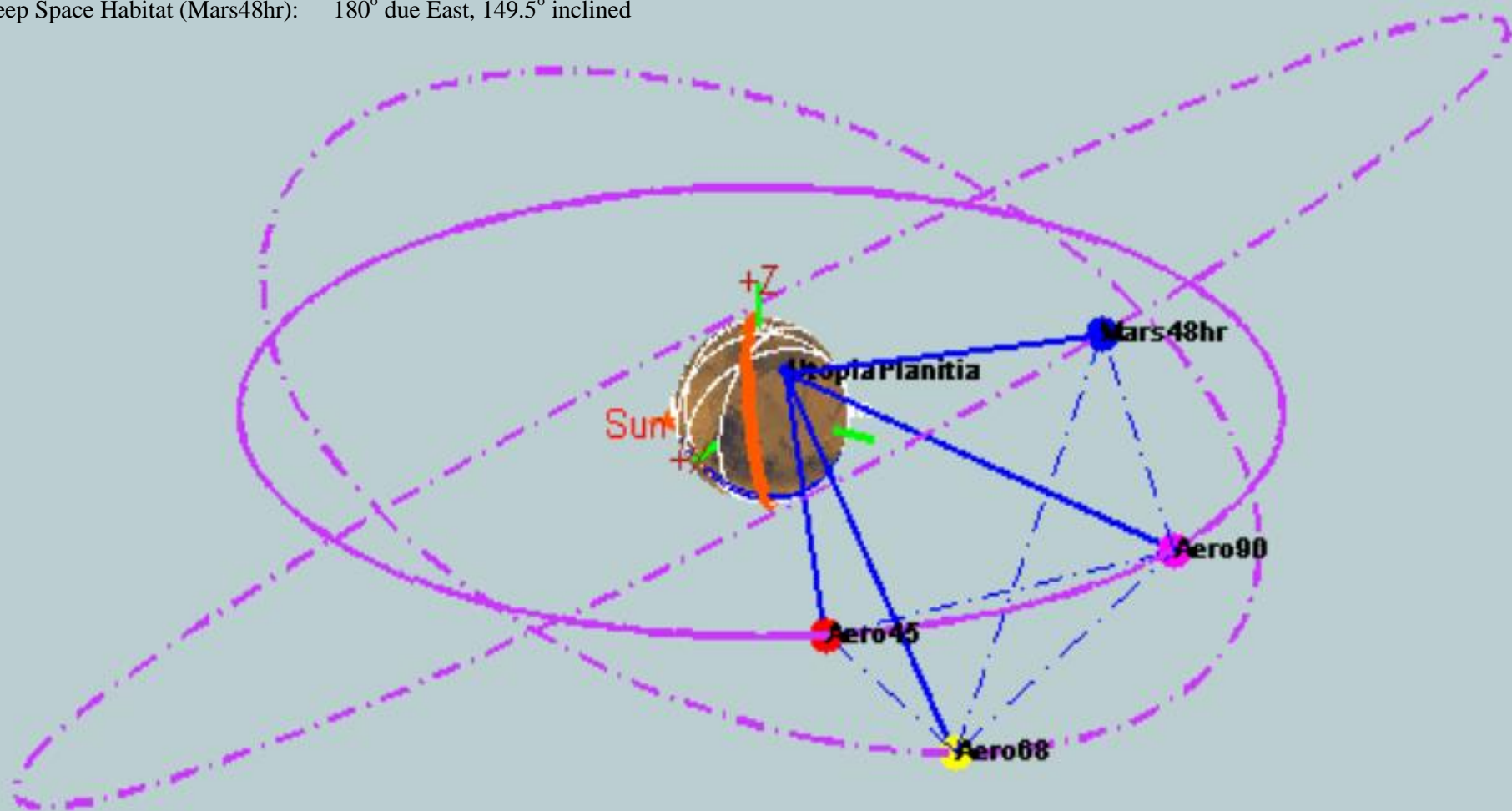


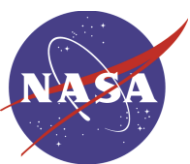
Mars Regional Navigation Satellite System (MRNSS) [8]

Orbits of the Notional Mars Navigation Nodes (3-D View)

Utopia Planitia: 182.5° due East, 46.7° due North
Aerostationary orbiter 1 (Aero45): 162.5° due East
Aerostationary orbiter 2 (Aero90): 207.5° due East
Aerosynchronous orbiter (Aero68): 180° due East and 20° inclined
Deep Space Habitat (Mars48hr): 180° due East, 149.5° inclined

?





Mars Regional Navigation Satellite System (MRNSS)

Preliminary Results on Localization Accuracy

| Our Proposed Scheme | | GPS Satellite Position Error | | | | | | | |
|---------------------|-------|------------------------------|---------|---------|----------|----------|----------|----------|----------|
| | | 0m | 0.5m | 1m | 2m | 5m | 10m | 30m | 35m |
| Pseudo-range error | 0.0m | 0.00 | 3273.85 | 6547.69 | 13095.39 | 32738.48 | 65476.99 | 196431.3 | 229169.9 |
| | 0.10m | 11.27 | 3273.70 | 6547.54 | 13095.23 | 32738.32 | 65476.82 | 196431.1 | 229169.7 |
| | 0.25m | 28.19 | 3273.56 | 6547.35 | 13095.01 | 32738.08 | 65476.58 | 196430.9 | 229169.5 |
| | 0.50m | 56.37 | 3273.51 | 6547.12 | 13094.89 | 32737.71 | 65476.19 | 196430.5 | 229169.1 |
| | 1.00m | 112.74 | 3274.15 | 6547.03 | 13094.24 | 32737.04 | 65475.45 | 196429.7 | 229168.3 |
| | 2.00m | 225.48 | 3278.35 | 6548.30 | 13094.06 | 32735.98 | 65474.10 | 196428.1 | 229166.7 |
| | 5.00m | 563.71 | 3313.95 | 6563.76 | 13099.34 | 32735.15 | 65471.23 | 196423.9 | 229162.4 |

Table 1. Absolute Localization Error Standard Deviation (cm) of the New Scheme. PDOP=113.17.

| Our Proposed Scheme | | GPS Satellite Position Error | | | | | | | |
|---------------------|-------|------------------------------|--------|--------|--------|--------|--------|---------|---------|
| | | 0m | 0.5m | 1m | 2m | 5m | 10m | 30m | 35m |
| Pseudo-range error | 0.0m | 14.43 | 21.57 | 35.07 | 65.44 | 160.06 | 319.04 | 956.04 | 1115.33 |
| | 0.10m | 21.59 | 26.82 | 38.47 | 67.27 | 160.75 | 319.32 | 956.05 | 1115.32 |
| | 0.25m | 42.77 | 45.58 | 53.22 | 76.58 | 164.76 | 321.27 | 956.58 | 1115.75 |
| | 0.50m | 81.89 | 83.33 | 87.69 | 103.45 | 178.67 | 328.48 | 958.82 | 1117.63 |
| | 1.00m | 161.95 | 162.62 | 164.84 | 173.61 | 226.38 | 356.41 | 968.34 | 1125.72 |
| | 2.00m | 323.00 | 323.28 | 324.34 | 328.78 | 359.12 | 452.05 | 1006.71 | 1158.71 |
| | 5.00m | 806.95 | 806.99 | 807.34 | 808.99 | 821.36 | 865.36 | 1246.30 | 1371.59 |

Table 2. Relative Localization Error Standard Deviation (cm) of the New Scheme.

Distance between Reference and Target = 100km. Sigma = 100m. Delta = 100m.


| Our Proposed Scheme | | GPS Satellite Position Error | | | | | | | |
|---------------------|-------|------------------------------|--------|--------|--------|--------|--------|--------|--------|
| | | 0m | 0.5m | 1m | 2m | 5m | 10m | 30m | 35m |
| Pseudo-range error | 0.0m | 0.14 | 1.59 | 3.18 | 6.35 | 15.87 | 31.73 | 95.20 | 111.07 |
| | 0.10m | 16.03 | 16.10 | 16.32 | 17.20 | 22.47 | 35.45 | 96.42 | 112.10 |
| | 0.25m | 40.08 | 40.10 | 40.18 | 40.53 | 42.99 | 50.93 | 103.02 | 117.79 |
| | 0.50m | 80.15 | 80.16 | 80.19 | 80.36 | 81.59 | 85.99 | 123.99 | 136.48 |
| | 1.00m | 160.31 | 160.30 | 160.32 | 160.39 | 160.97 | 163.19 | 185.83 | 194.34 |
| | 2.00m | 320.62 | 320.61 | 320.61 | 320.63 | 320.89 | 321.95 | 333.77 | 338.52 |
| | 5.00m | 801.54 | 801.53 | 801.52 | 801.52 | 801.58 | 801.93 | 806.47 | 808.38 |

Table 3. Relative Localization Error Standard Deviation (cm) of the New Scheme.

Distance between Reference and Target = 10km. Sigma = 100m. Delta = 100m.

200 – 400 folds
improvement
in RMSE accuracy

Sigma: media delay
Delta: clock bias

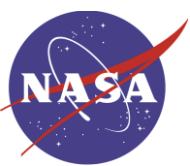


Simultaneous 2-Way Communications/Doppler/Ranging: System Approach

- Assume X-band, which supports low rate commands/telemetry
- The Mars orbiters all lie within the same beamwidth of a DSN 34-m BWG antenna
- For N orbiters, the downlinks operate in N allocated frequency bands separated by $N-1$ guard bands to prevent interference
- Flight and ground upgrades:
 - The N orbiters time-share a single uplink; commands differentiated by SCID (MUPA) [9]
 - The ground “Doppler-compensates” the uplink carrier signal in either way:
 - With respect to the Mars center
 - With respect to the average (centroid) of Doppler’s of N orbiters

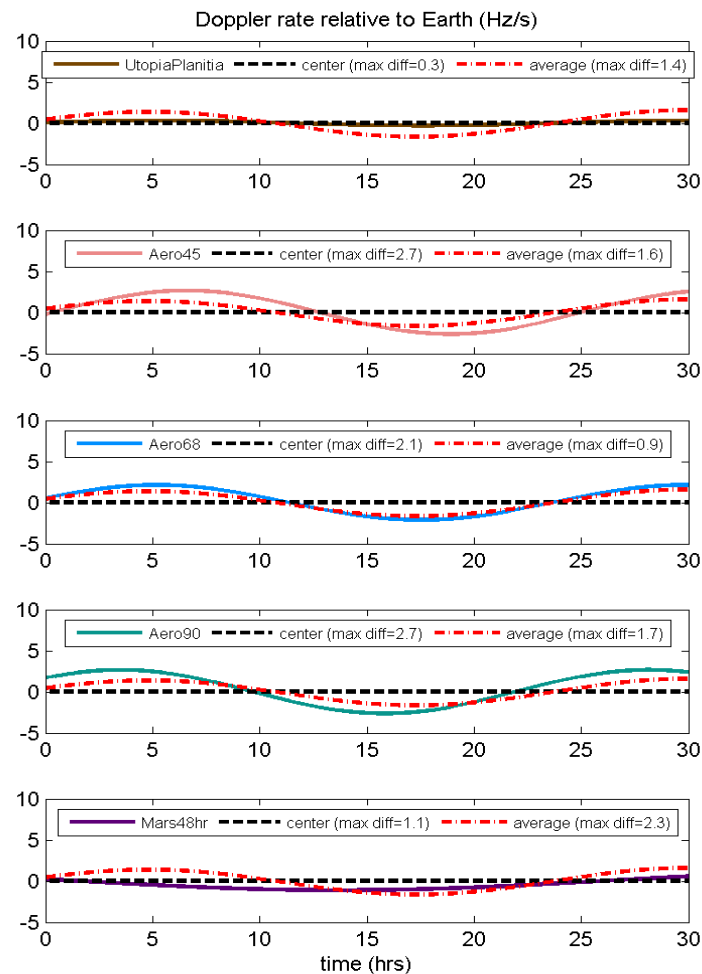
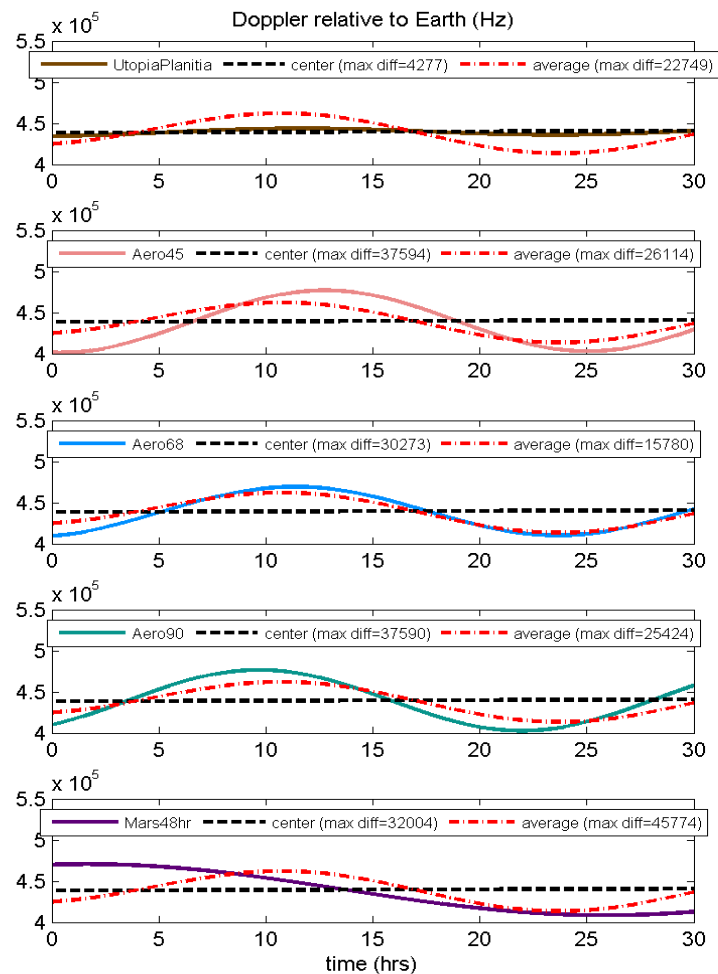
Guard bands must be wide enough to accommodate the residual Doppler. Preliminary simulations: residual Doppler and Doppler rate are bounded by 45 KHz & 2.6 Hz/s

- Flight radio upgrades:
 - A different turn-around-ratio for each spacecraft so the same uplink would be coherently “turned-around” to modulate the telemetry and ranging signals on a different allocated downlink frequency
 - A well-designed tracking loop that can sweep, acquire, and track the unknown uplink carrier phase and high residual Doppler frequency
- Ground station uses existing MSPA for telemetry/Doppler/range processing



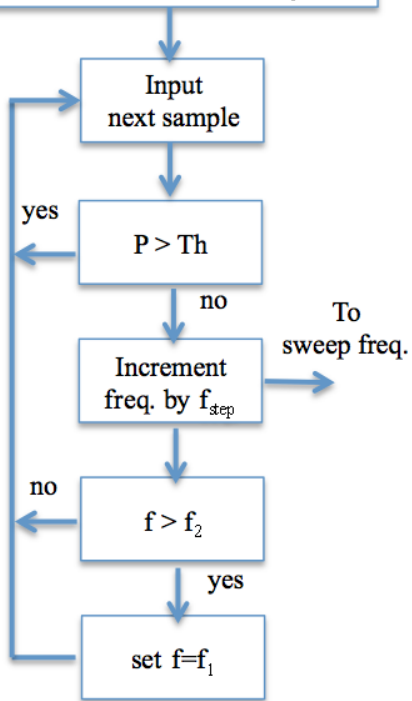
Simultaneous 2-Way Communications/Doppler/Ranging

Doppler and Doppler Rate Profiles

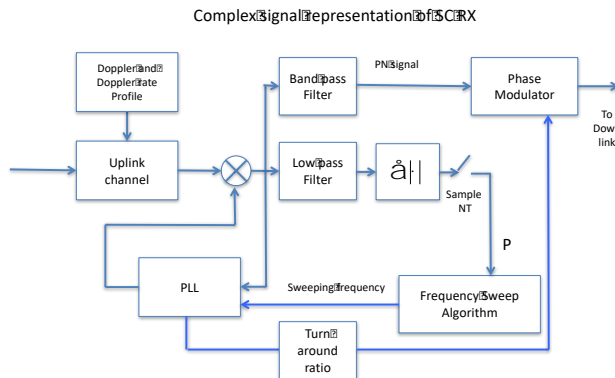
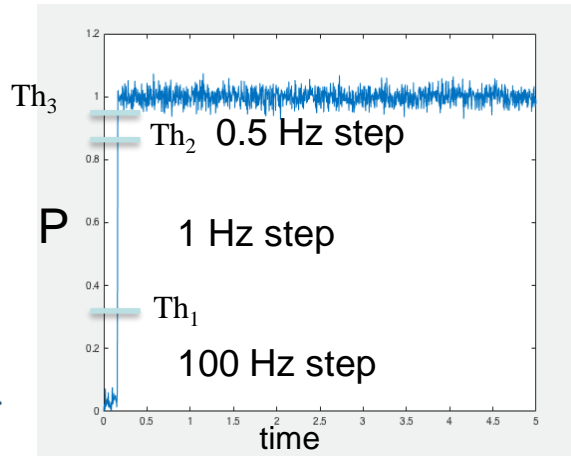


Simultaneous 2-Way Communications/Doppler/Ranging: Smart PLL Tracking

Initialize sweep freq., set initial freq. f_1 , final freq. f_2 , step freq. f_{step} , Th

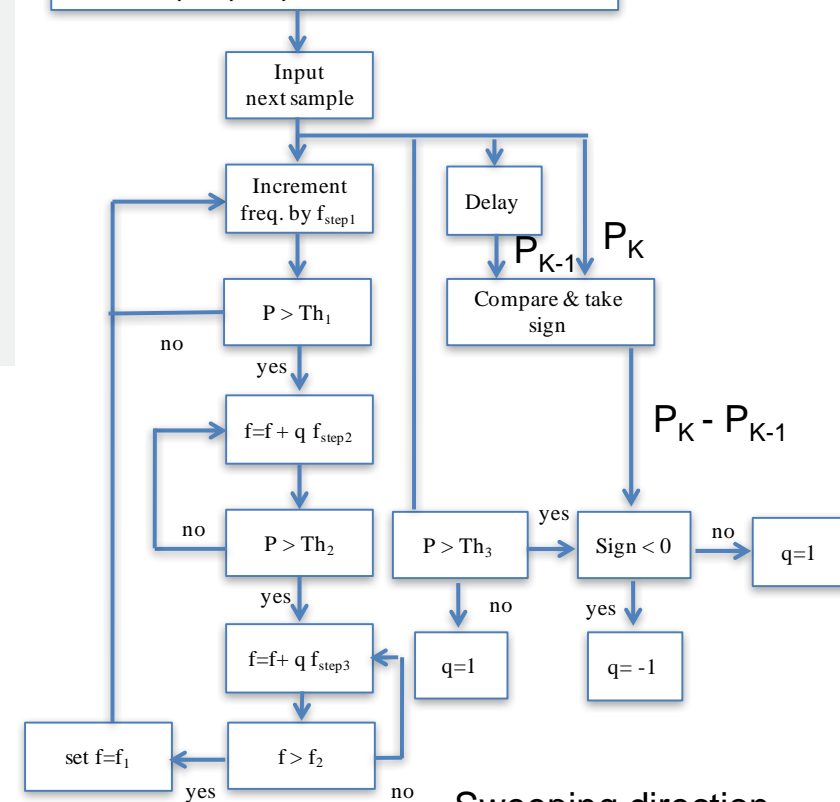


Current straight-forward
Electra sweeping algorithm



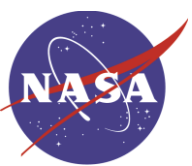
A new frequency sweep acquisition algorithm

Initialize sweep freq., set initial freq. f_1 , final freq. f_2 , step freq. f_{step1} , f_{step2} , f_{step3} , and thresholds Th_1, Th_2, Th_3



Dynamic sweeping circuit

Sweeping direction
estimation circuit

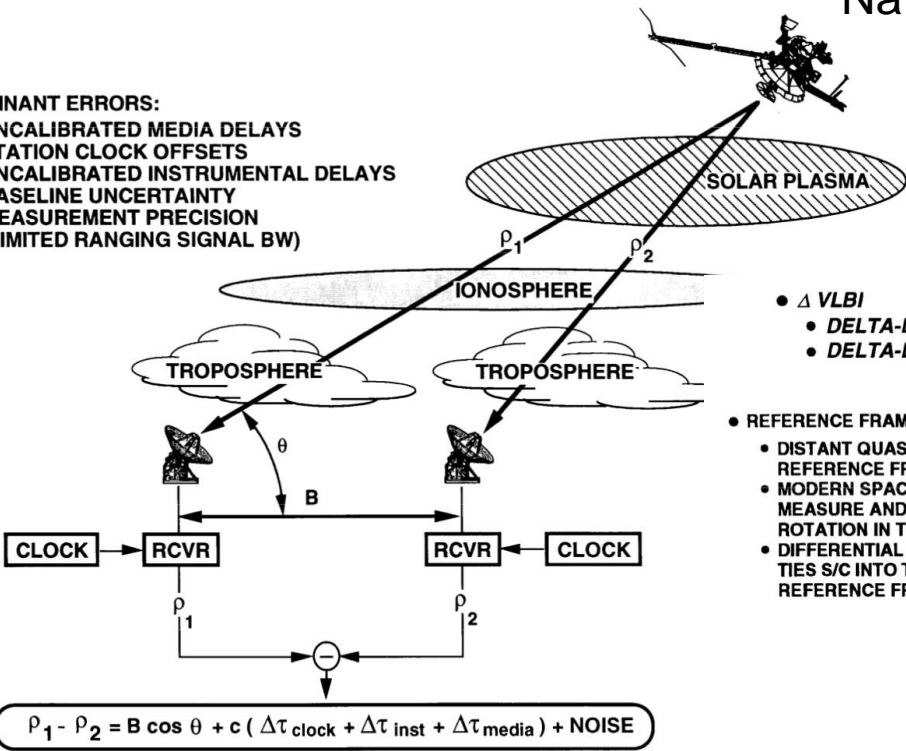


Simultaneous Delta-DOR: Theory of Delta-DOR

Diagrams from “The Evolution of Deep Space Navigation: 1962-1989,” by Lincoln Wood

• DOMINANT ERRORS:

- UNCALIBRATED MEDIA DELAYS
- STATION CLOCK OFFSETS
- UNCALIBRATED INSTRUMENTAL DELAYS
- BASELINE UNCERTAINTY
- MEASUREMENT PRECISION (LIMITED RANGING SIGNAL BW)

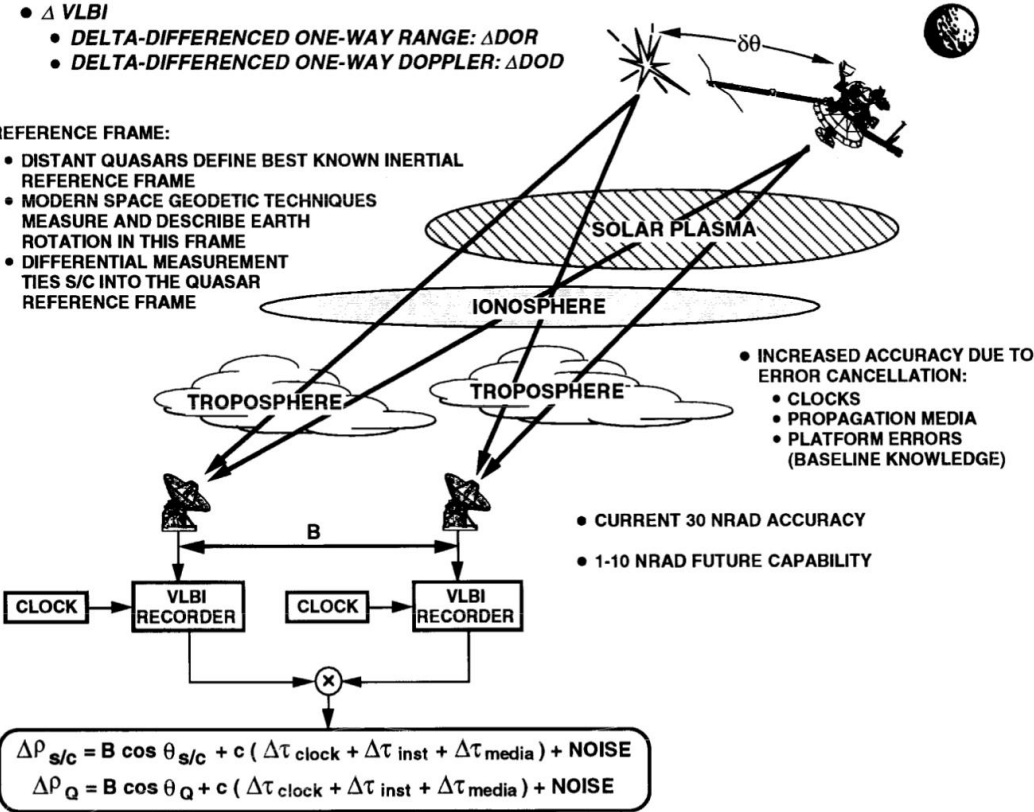


• Δ VLBI

- DELTA-DIFFERENCED ONE-WAY RANGE: ΔDOR
- DELTA-DIFFERENCED ONE-WAY DOPPLER: ΔDOD

• REFERENCE FRAME:

- DISTANT QUASARS DEFINE BEST KNOWN INERTIAL REFERENCE FRAME
- MODERN SPACE GEODETIC TECHNIQUES MEASURE AND DESCRIBE EARTH ROTATION IN THIS FRAME
- DIFFERENTIAL MEASUREMENT TIES S/C INTO THE QUASAR REFERENCE FRAME



• INCREASED ACCURACY DUE TO ERROR CANCELLATION:

- CLOCKS
- PROPAGATION MEDIA
- PLATFORM ERRORS (BASELINE KNOWLEDGE)

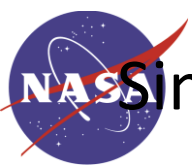
• CURRENT 30 NRAD ACCURACY

• 1-10 NRAD FUTURE CAPABILITY



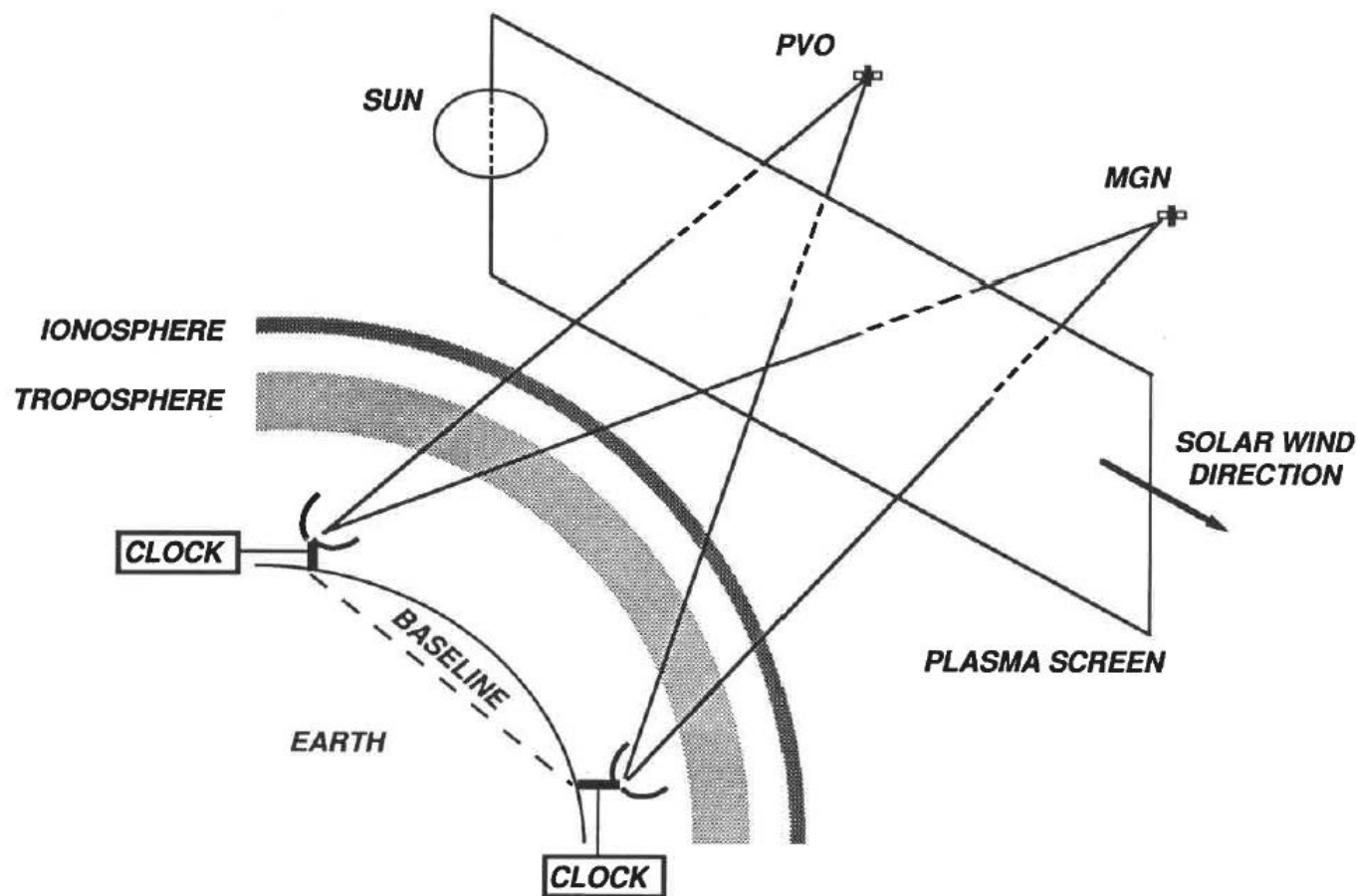
Simultaneous Delta-DOR: Same Beam Interferometry (1)

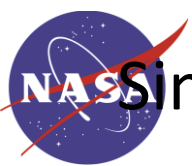
- Same Beam Interferometry (SBI) was proposed by Jim Border et. al. to support the tracking of the Magellan and the Pioneer Venus orbiters over 25 years ago [7]
- Like Delta-DOR, SBI uses double-differencing of signal arrival times to achieve highly accurate angular distance estimation
 - Eliminate clock biases, media delay, instrument delays, etc.
- Instead of using quasar as reference (5- 6 degree away), one can use a nearby spacecraft as a reference (less than a milli-degree)
 - Ground antennas do not need to point back-and-forth between the quasar and the spacecraft, thus increase observation time and simplify operation
 - Angular distance between spacecraft is much closer, thus increase accuracy from 10's nano-radian to nano-radians
- Quasar calibrations are needed only at the beginning and at the end of an overlapping pass



Simultaneous Delta-DOR: Same Beam Interferometry (2)

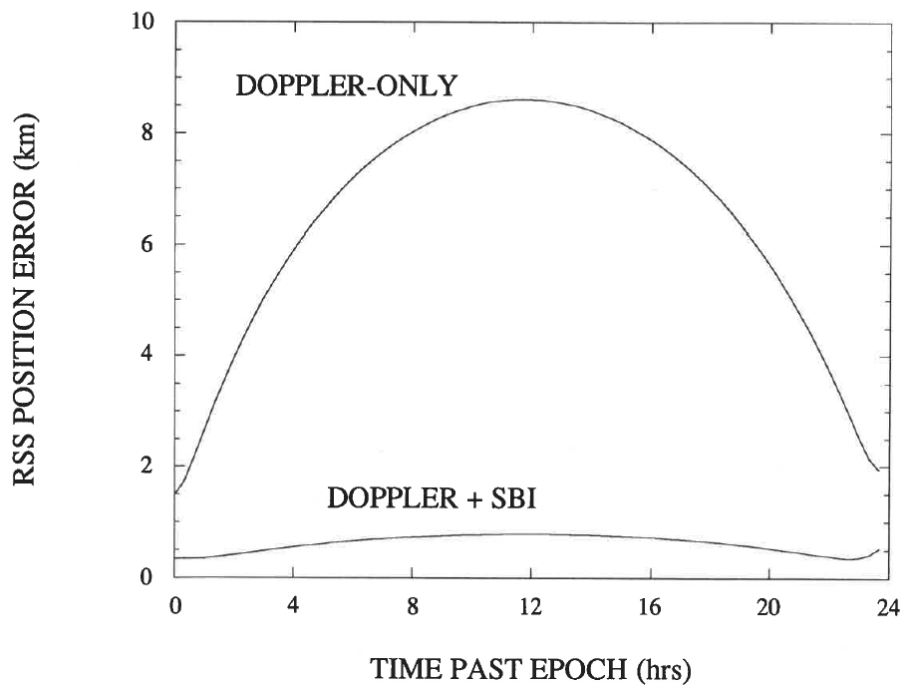
SAME-BEAM INTERFEROMETRY ERROR SOURCES



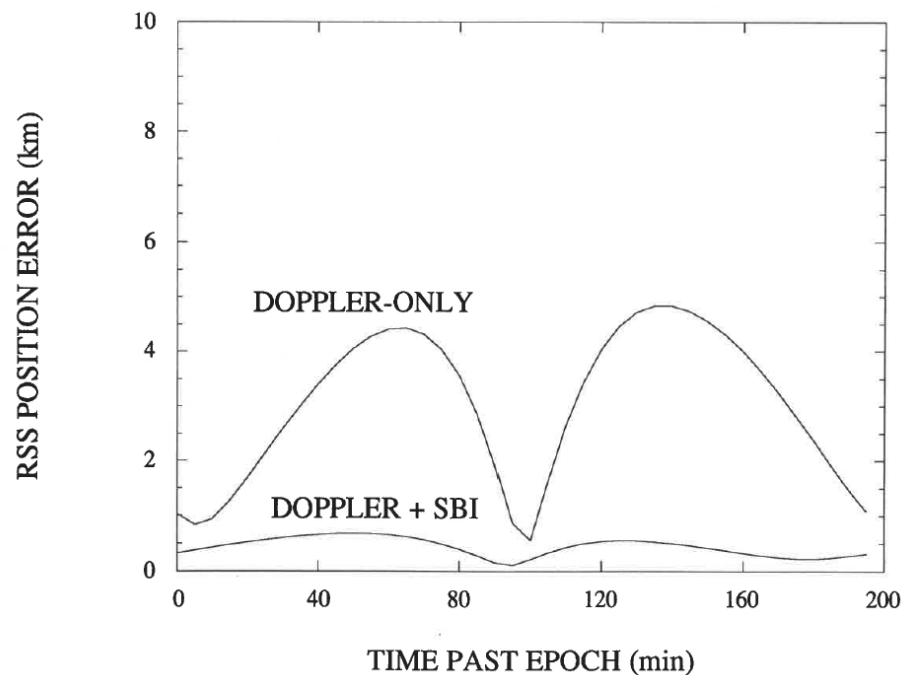


Simultaneous Delta-DOR: Same Beam Interferometry (3)

PVO ORBIT ACCURACY - PREDICTED
AUGUST 11, 1990



MGN ORBIT ACCURACY - PREDICTED
AUGUST 11, 1990



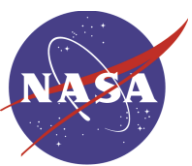


Simultaneous Delta-DOR: Same Beam Interferometry (4)

- SBI is more accurate, and operationally simpler than Delta-DOR
- Since the introduction of SBI, SBI was used or proposed for use in some deep space (including lunar) scenarios, e.g. approach/landing, ascent/docking, etc.

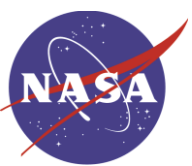
Examples:

- Q. Liu, F. Kikuchi, K. Matsumoto, et. al., “Error Analysis of Same-Beam Differential VLBI Technique using two SELENE satellites,” *Advances in Space Research* 40 (2007).
- M. Chen, Q. Liu, “Study on Differential Phase Delay Closure of Same-Beam VLBI,” 2nd International Conference on Computer Engineering and Technology, April 2010, Chengdu, China
- S. Chen, Q. Liu, “A Study on Accurate Same Beam Interferometry Differential Phase Delay Closure,” 12th International Conference on Computer and Information Technology, October 2012, Chengdu, China
- T. Martin-Mur, D. Highsmith, “Mars Approach Navigation Using the VLBA,” *Proceedings of the 21st International Symposium on Space Flight Dynamics*, Toulouse, France, September 28 – October 2, 2009



Can this Enable New Mission Concept and Science?

- An exercise of a solution looking for the right problems...
- This new “Multiple spacecraft per antenna” approach enables simultaneous communications, Doppler, ranging, and “delta-DOR” with different spacecraft, thus greatly reduces the burden of ground network. But can this approach also enable new mission concepts and science?
- Multiple spacecraft (CubeSats?) orbiting a moon or a planet to provide simultaneous Doppler measurements
 - Spacecraft life-time limitation, e.g. Class-D CubeSats, spacecraft at the harsh radiation environment of Jupiter
 - Short operation duration and graceful degradation
 - Spatial diversity of measurements to study system dynamics – gravity, atmosphere, and magnetic field
- Any ideas?



References

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- [2] Mars Architecture Steering Group, Human Exploration of Mars Design Reference Architecture 5.0, Technical Report, NASA, 2009.
- [3] D. Bell, R. Cesarone, T. Ely, C. Edwards, S. Townes, “MarsNet: A Mars Orbiting Communications & Navigation Satellite Constellation,” IEEE Aerospace Conference 2000, March 2000, Big Sky, Montana.
- [4] K. Cheung, C. Lee, A Trilateration Scheme for Relative Positioning, IEEE Aerospace Conference 2017, Big Sky, Montana, March 2017.
- [5] K. Cheung, C. Lee, “A Trilateration Scheme for GPS-Style Localization,” Interplanetary Network Progress Report, 42-209, May 15, 2017.
- [6] K. Cheung, D. Divsalar, S. Bryant, and C. Lee, “Simultaneous 2-Way Doppler and Ranging for Multiple Spacecraft at Mars,” IEEE Aerospace Conference 2018, Big Sky, Montana, March 2018.
- [7] J. Border, W. Folkner, R. Kahn, and K. Zukor, “Precise Tracking of the Megellan and Pioneer Venus Orbiters by Same-Beam Interferometry, Part I: Data Accuracy Analysis,” Interplanetary Network Progress Report, 42-110, August 15, 1992.
- [8] K. Cheung, C. Lee, “In-Situ Navigation and Timing Services for a Human Mars Landing Site Part 1: System Concept,” September 2017, 68th International Astronautical Congress, Adelaide, Australia.
- [9] D. Abraham, B. MacNeal, D. Heckman, Enabling Affordable Communications for the Burgeoning Deep Space CubeSat Fleet, SpaceOps 2016, May 2016, Daejeon, Korea.